

V393  
.R46

MIT LIBRARIES



3 9080 02753 0788



DEPARTMENT OF THE NAVY



HYDROMECHANICS

COMPUTER PROGRAM DOCUMENTATION

STEAM CONDENSER DESIGN

AERODYNAMICS

by

STRUCTURAL  
MECHANICS



M. Botting

D. Kelly

Distribution of this document is unlimited

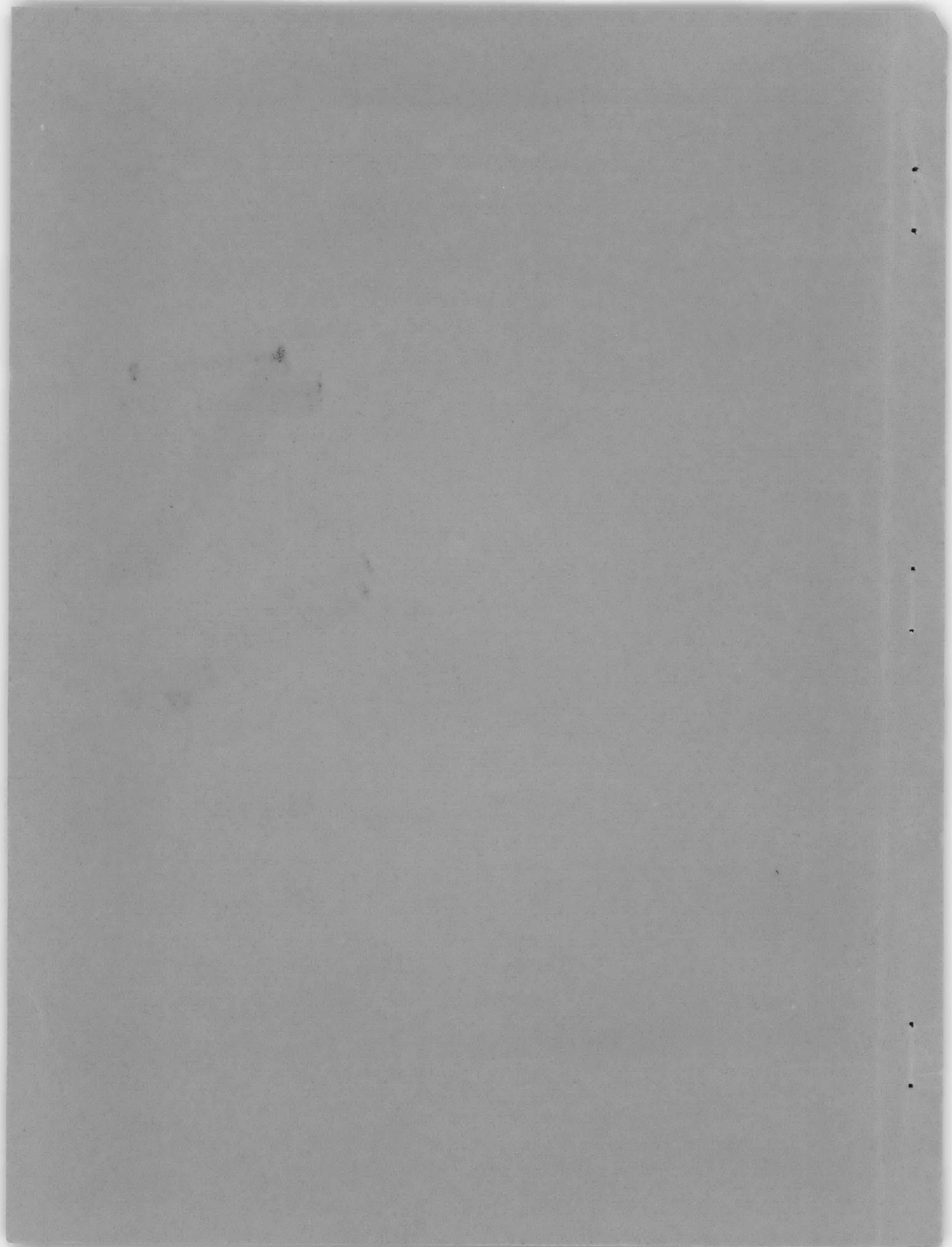
APPLIED  
MATHEMATICS

APPLIED MATHEMATICS LABORATORY  
RESEARCH AND DEVELOPMENT REPORT

ACOUSTICS AND  
VIBRATION

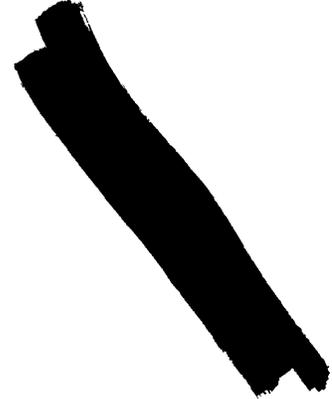
July 1966

Report 2255



**COMPUTER PROGRAM DOCUMENTATION**  
**STEAM CONDENSER DESIGN**

by



**M. Botting**

**D. Kelly**

**Distribution of this document is unlimited**

**July 1966**

**Report 2255**  
**SR003-0801**  
**Task 10894**

## TABLE OF CONTENTS

	Page
ADMINISTRATIVE INFORMATION . . . . .	1
I. IDENTIFICATION DATA . . . . .	2
II. PURPOSE AND METHOD . . . . .	5
III. RESTRICTIONS . . . . .	8
IV. NON-STANDARD OPERATING INSTRUCTIONS . . . . .	9
V. DATA PREPARATION . . . . .	10
VI. CONTROL INFORMATION . . . . .	24
VII. ACKNOWLEDGMENT . . . . .	58
REFERENCES . . . . .	59

## ADMINISTRATIVE INFORMATION

This work was accomplished under project SR003-0801, Task 10894.

The Computer program and documentation herein has been approved by the Naval Ship Engineering Center for use in naval ship design.

The U. S. Government will incur no liability for loss arising from the use of the computer program described herein.

**I. IDENTIFICATION DATA**

**A. Title - Steam Condenser Design**

- 1. FORTRAN IV Deckname - COND
- 2. Revision - A - Original Issue

**B. Abstract - This program calculates all the necessary information required for the selection of main or auxiliary steam condensers to either preliminary or contract design requirements.**

For preliminary design a graph is also provided which relates condenser overall length with tube sheet diameter for a specified set of design conditions. For contract design a graph relating condenser absolute pressure and increments of heat rejection at integer circulating water velocities is also provided for analysis of part load performance.

**C. Input/Calculated Items/Output**

**1. Input**

<u>Term</u>	<u>Standard Symbol</u>
Tube Material	XMA1TU
Tube Gage	GA1TU
Tube Outside Diameter (inches)	D5TU
Number of Passes	XN2PS
Cleanliness Factor	F2TCLN
Number of Tube Sheets per end	XN2TSE
Ineffective Tube Length per end (inches)	XL1TUI

<u>Term</u>	<u>Standard Symbol</u>
Tube Hole Space Factor	F2TUHO
Steam Flow to Condenser (lb/hr)	R9SF5
Heat Rejected per pound of Steam (BTU/lb)	HTISR
Design Back Pressure (inches-hg)	P2BDES
Injection Water Temperature ( <sup>o</sup> F.)	TEIINJ
Overall Condenser Length Desired (ft)	XLITT
Desired Diameter of Tube Sheet (ft)	D5COND
Circulating Water Velocity in Tubes (ft/sec)	VIWTU
Ordered Tube Length Shortest	XLITUO
Ordered Tube Length Longest	QLITUO

2. Internal Values

<u>Term</u>	<u>Standard Symbol</u>
Tube Wall Thickness	TH1TU
Basic Heat Transfer Coefficient	C1HEAT
Tube Constant	C9TU
Material and Gage Factor	F2MG
Temperature Correction Factor	F2TEC
GPM/1 FPS/Tube	F1V6TU

3. Output

<u>Term</u>	<u>Standard Symbol</u>
Temperature Saturated Liquid	TEISAT
Ordered Tube Length	XLITUO
Tube Surface Area	S2TU

<u>Term</u>	<u>Standard Symbol</u>
Effective Tube Length	XL1TUE
Number of Tubes	XN2TUT
Tube Sheet Diameter	D5TUSH
Tube Sheet Area	ALTUSH
Overall Condenser Length	XL1CON
Circulating Water Required (GPM)	R9SW2
Circulating Water Outlet Temp.	TE1O
Terminal Temperature Diff.	TE1TD
Circulating Water Temperature Rise	TE1R

D. Author/Date

Maxine Botting    Denis Kelly    December 1965

E. Organization

Computer-Aided Ship Design Division, Code 850, David Taylor  
Model Basin.

F. Computer/Source Language

IBM 7090    FORTRAN IV    CARD INPUT

G. Reference to Documentation

DTMB Report 2255 of July 1966

H. Security Classification

Unclassified

I. Estimated Running Time

1 1/2 minutes.

## II. PURPOSE AND METHOD

### A. Description of Method

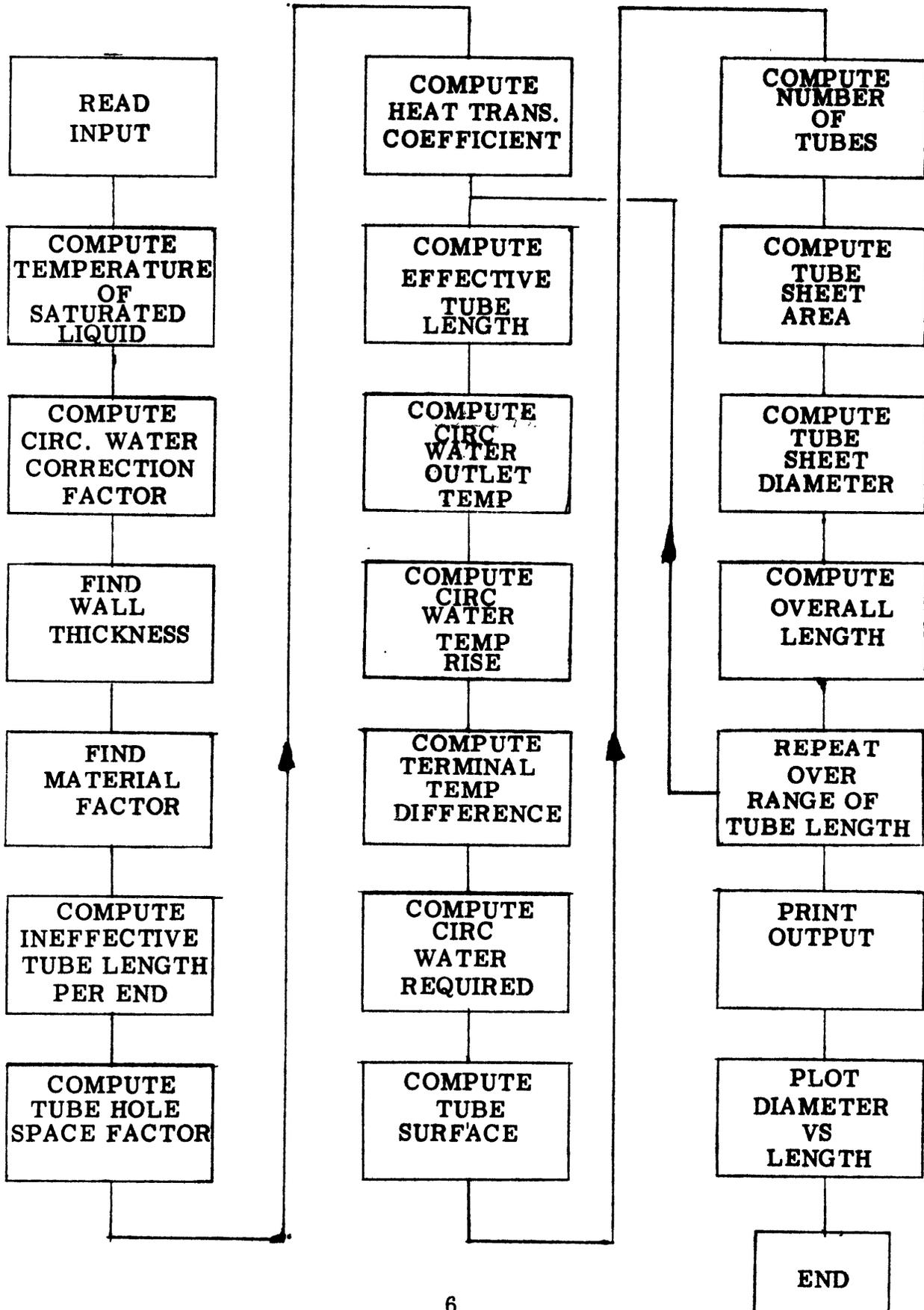
The purpose of this program is to develop the required design data necessary for the selection of a steam condenser in accordance with the ordering data specified in military specification MIL-C-15430G. Since any condenser design is a balance of tube surface, tube length and cooling water quantity, it is the space allowed for the condenser that actually is the deciding factor in the design. If the limiting dimensions are known the contract design mode is employed and the design is calculated based on these specific dimensions. If exact limiting dimensions are not known, a range of tube lengths can be specified, the preliminary design mode employed, and a number of satisfactory designs reviewed.

The theory and formulations of the design process are shown in design data sheet DDS4601-1 of 15 October 1953.

The temperature of a saturated liquid as a function of pressure and pressure as a function of temperature are obtained by formulations developed by Westinghouse Corporation based on Keenan and Keyes values.

A simple descriptive flow chart is as follows:

PRELIMINARY DESIGN MODE



## **Contract Design Mode**

In the contract design mode an estimated ordered tube length is computed based on the overall condenser length used as input. The above calculations are then performed and a calculated overall length developed. This value is compared with the desired overall length. If larger the ordered tube length is incremented six inches smaller and the calculations repeated. When the calculated length is equal or smaller the program then checks the tube sheet diameter. If the calculated value is too large the program stops. If it is satisfactory a plot of heat load versus absolute pressure is developed for various circulating water velocities from input value down to 3 feet/sec.

### **B. Assumptions**

Tube materials and gage factors for 12 and 13 BWG are extrapolated from HEI standards for steam surface condensers which include only 14-18 BWG.

### **C. References**

1. Design Data Sheet DDS4601-1 of 15 October 1953 - Steam Condensers.
2. Military Specification MIL-C-15430G Condensers, Steam Surface, Naval Shipboard.
3. Share Programs C3-WH58-PA-3137 (Westinghouse Corporation Properties of Steam).

### III. RESTRICTIONS

A. Non-standard subroutines not included in the program are the North American S-C 4020 subroutine package.

B. A tape is required on B-9 to go to the S-C 4020.

C. Non-standard hardware is the S-C 4020.

D. Maximum Array Size

In the preliminary design mode there is a limit of 10 tube lengths starting with the shortest and increasing at six inch intervals.

#### IV. NON-STANDARD OPERATING INSTRUCTIONS

- A. There are no special operating instructions.
- B. There are no restart instructions.
- C. There are no on line error corrections.
- D. Validation Checks

The program has been checked and found to be accurate against the sample problems contained in design data sheet DDS4601-1 of 15 October 1953.

## V. DATA PREPARATION

### A. Card Input Description

All input except the first card is a 12 column fields. The specified columns are where a typical value would be. Decimal points are necessary and all values should be right adjusted.

For limitations on input see VI-C- SPECIAL DIAGNOSTICS.

<u>CARD</u>	<u>DATA</u>	<u>TYPICAL FIELD</u>	<u>INPUT PARAMETERS</u>	<u>COLUMNS</u>
First	Title for output (Must be centered in field to be cen- tered on output)			1 - 72
Second	(Tube Material)	X.	1. (70 - 30 CU-NI) 2. ( 90 - 10 CU-NI)	11 - 12
Second	(Tube Gage)	XX.	12 to 18	22 - 24
Second	(Tube Diameter)	.XXX	.625 .750 .875	33 - 36
Second	(Cleanliness Factor)	.XX	.85 (Typical Value)	46 - 48
Second	(No. of Tube Sheets/ end)	X.	1. or 2.	59 - 60
Second	(Ineffective Tube Length per end)	X.	If 0 program will calculate this value	71 - 72
Third	(Tube Hole Space Factor)	X.XX	If 0 program will calculate this value	9 - 12
Third	(No. of passes)	X.		23 - 24
Third	(Steam to Condenser)	XXXXXXXX.		30 - 36
Third	(Heat Rejected	XXX.		45 - 48
Third	(Design Back Pressure)	XX.X		57 - 60

<u>CARD</u>	<u>DATA</u>	<u>TYPICAL FIELD</u>	<u>INPUT PARAMETERS</u>	<u>COLUMN</u>
Third	(Circ. Water Velocity)	XX.		70 - 72
Fourth	(Injection water temperature)	XX.		10 - 12
Fourth	(Desired overall condenser length)	XX.X	If 0 will execute preliminary design If a value will execute contract design	21 - 24
Fourth	(Desired diameter of tube sheet)	XX.X		33 - 36
Fourth	(Shortest ordered tube length)	XX.X	} Must be 10 values or less at 6 inch intervals between shortest and longest ordered tube length	57 - 60
Fourth	(Longest ordered tube length)	XX.X		





### **C. Output Form Description**

The input data is printed as the first output in each mode. In the preliminary design mode the desired overall condenser length and tube sheet diameter values are zero. The calculated output is self-explanatory for each mode. Graphic output for the preliminary mode shows the relationship between circular tube sheet diameter and overall condenser length for a given set of design conditions. Graphic output for the contract design mode shows condenser part load performance with the condenser absolute pressure and heat rejection load (up to 110% of full power) shown at various circulating water velocities.

## TEST CASE 1

## CONDENSER DESIGN PROGRAM

## INPUT VALUES

TUBE MATERIAL	90-10
TUBE GAGE	18.
TUBE DIAMETER (IN)	0.6250
CLEANLINESS FACTOR	0.8500
NUMBER OF TUBE SHEETS PER END	1.
INEFFECTIVE TUBE LENGTH PER END (IN)	0.
TUBE HOLE SPACE FACTOR	0.
NUMBER OF PASSES	1.
STEAM TO CONDENSER (LB/HR)	217000.
HEAT REJECTED PER POUND OF STEAM (BTU/LB)	936.00
DESIGN BACK PRESSURE (IN HG)	5.00
CIRC WATER VELOCITY IN TUBES (FT/SEC)	9.00
INJECTION WATER TEMPERATURE (DEG F)	75.00
DESIRED OVERALL CONDENSER LENGTH (FT)	0.
DESIRED DIAMETER OF TUBE SHEET (FT)	0.
ORDERED TUBE LENGTH SHORTEST (FT)	9.00
ORDERED TUBE LENGTH LONGEST (FT)	12.00

15

V. D-1 SAMPLE OUTPUT  
PRELIMINARY DESIGN MODE

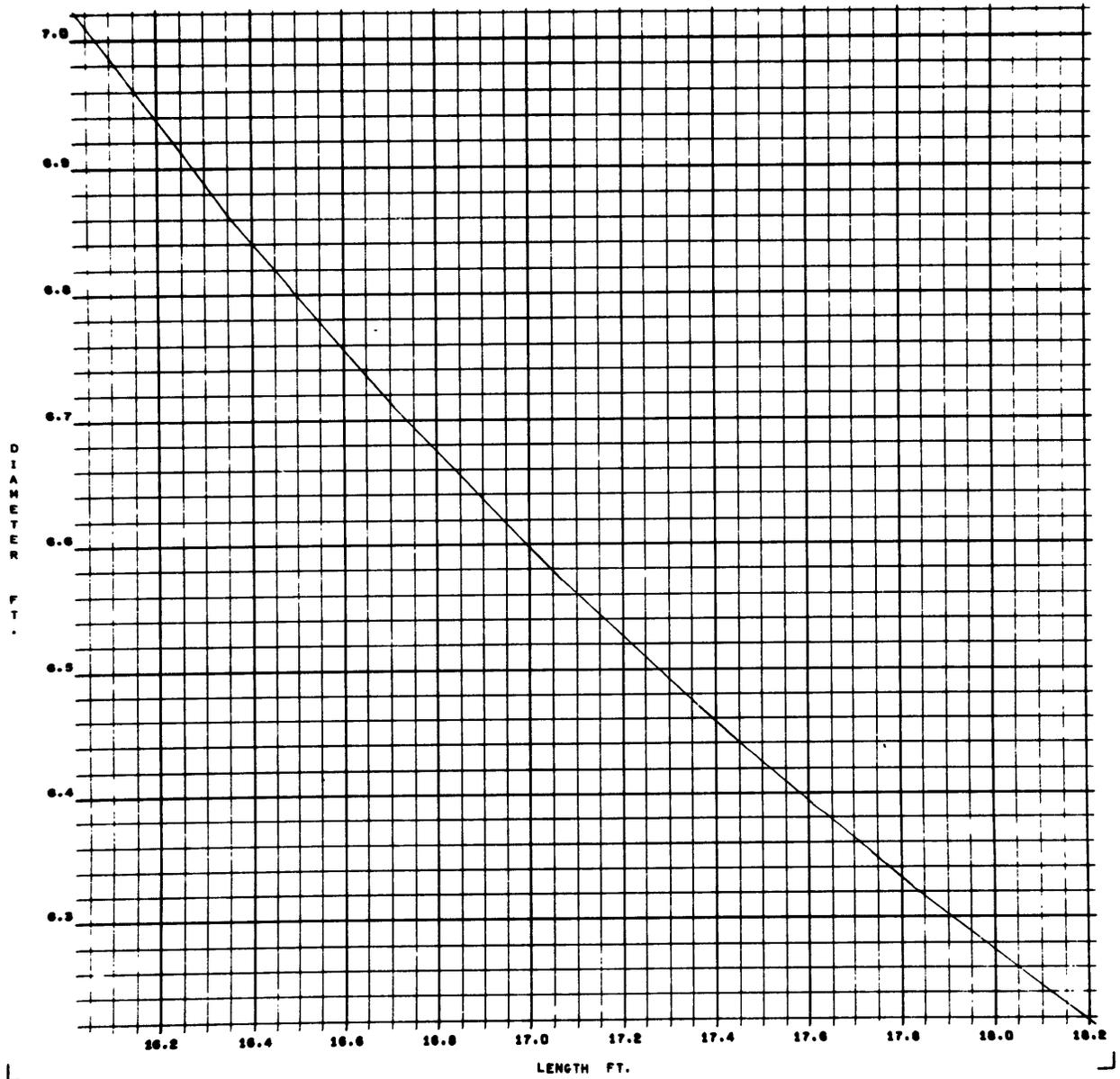
CUTPUT VALUES

	TEMPERATURE SATURATED LIQUID (DEG F)			133.7590				
	ORDERED TUBE LENGTH (FT)	9.00	9.50	10.00	10.50	11.00	11.50	12.00
	TUBE SURFACE AREA (SQ FT)	6299.	6350.	6401.	6452.	6504.	6556.	6608.
	EFFECTIVE TUBE LENGTH (FT)	8.82	9.32	9.82	10.32	10.82	11.32	11.82
	NUMBER OF TUBES	4364.	4163.	3983.	3820.	3673.	3539.	3416.
	TUBE SHEET DIAMETER (FT)	7.02	6.86	6.71	6.57	6.44	6.32	6.21
	TUBE SHEET AREA (SQ FT)	38.74	36.96	35.36	33.91	32.61	31.42	30.32
	OVERALL CONDENSER LENGTH (FT)	16.02	16.36	16.71	17.07	17.44	17.82	18.21
16	CIRCULATING WATER REQD (GPM)	26697.	25469.	24368.	23374.	22473.	21652.	20902.
	CIRC WATER OUTLET TEMP (DEG F)	90.22	90.95	91.67	92.38	93.08	93.76	94.43
	TERMINAL TEMP DIFF (DEG F)	43.54	42.81	42.09	41.38	40.68	40.00	39.32
	CIRC WATER TEMP RISE (DEG F)	15.22	15.95	16.67	17.38	18.08	18.76	19.43

V. D-1 SAMPLE OUTPUT  
PRELIMINARY DESIGN MODE

V. D-1 SAMPLE OUTPUT  
PRELIMINARY DESIGN MODE

TEST CASE 1 CONDENSER DESIGN PROGRAM



## INPUT VALUES

18

TUBE MATERIAL	90-10
TUBE GAGE	18.
TUBE DIAMETER (IN)	0.6250
CLEANLINESS FACTOR	0.8500
NUMBER OF TUBE SHEETS PER END	1.
INEFFECTIVE TUBE LENGTH PER END (IN)	0.
TUBE HOLE SPACE FACTOR	0.
NUMBER OF PASSES	1.
STEAM TO CONDENSER (LB/HR)	217000.
HEAT REJECTED PER POUND OF STEAM (BTU/LB)	936.00
DESIGN BACK PRESSURE (IN HG)	5.00
CIRC WATER VELOCITY IN TUBES (FT/SEC)	9.00
INJECTION WATER TEMPERATURE (DEG F)	75.00
DESIRED OVERALL CONDENSER LENGTH (FT)	18.00
DESIRED DIAMETER OF TUBE SHEET (FT)	10.00
ORDERED TUBE LENGTH SHORTEST (FT)	0.
ORDERED TUBE LENGTH LONGEST (FT)	0.

V. D-2 SAMPLE OUTPUT  
CONTRACT DESIGN MODE

OUTPUT VALUES

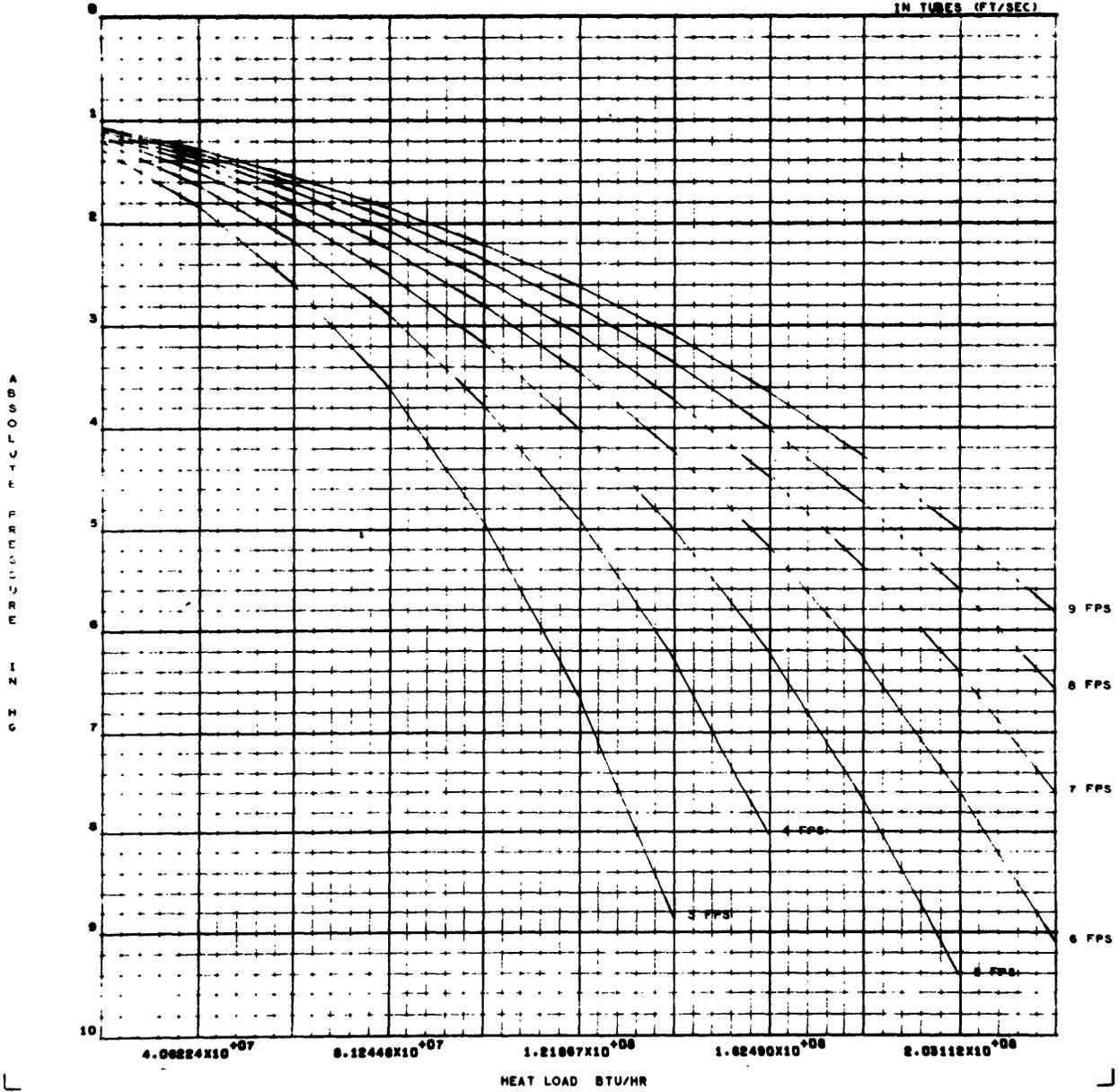
TEMPERATURE SATURATED LIQUID (DEG F)	133.7590
ORDERED TUBE LENGTH (FT)	11.50
TUBE SURFACE AREA (SQ FT)	6556.
EFFECTIVE TUBE LENGTH (FT)	11.32
NUMBER OF TUBES	3539.
TUBE SHEET DIAMETER (FT)	6.32
TUBE SHEET AREA (SQ FT)	31.42
OVERALL CONDENSER LENGTH (FT)	17.82
19 CIRCULATING WATER REQD (GPM)	21652.
CIRC WATER OUTLET TEMP (DEG F)	93.76
TERMINAL TEMP DIFF (DEG F)	40.00
CIRC WATER TEMP RISE (DEG F)	18.76

V. D-2 SAMPLE OUTPUT  
CONTRACT DESIGN MODE

# V. D-2 SAMPLE OUTPUT CONTRACT DESIGN MODE

TEST CASE 2 CONDENSER DESIGN PROGRAM

CIRC WATER VELOCITY  
IN TUBES (FT/SEC)



## E. Symbol List

See list in I. C.

## F. Data Tables Used by Program

### 1. Factors used in determining saturated liquid temperature:

#### Reference (3)

(QAA)	$A_0 = 35.15789$
	$A_1 = 24.592588$
	$A_2 = 2.1182069$
	$A_3 = -.3414474$
	$A_4 = .15741642$
	$A_5 = -.031329585$
	$A_6 = .0038658282$
	$A_7 = -.00024901784$
	$A_8 = .0000068401559$

### 2. Circulating Water Temperature Correction Factors:

#### Reference (1)

(QCF)	$30^{\circ}\text{F} = .65$
	$35^{\circ}\text{F} = .70$
	$40^{\circ}\text{F} = .75$
	$45^{\circ}\text{F} = .798$
	$50^{\circ}\text{F} = .843$
	$55^{\circ}\text{F} = .886$
	$60^{\circ}\text{F} = .926$

(QCF)	65 <sup>o</sup> F = .963
	70 <sup>o</sup> F = 1.0
	75 <sup>o</sup> F = 1.025
	80 <sup>o</sup> F = 1.045
	85 <sup>o</sup> F = 1.061
	90 <sup>o</sup> F = 1.076
	95 <sup>o</sup> F = 1.09
	100 <sup>o</sup> F = 1.1

3. Wall Thickness Factors: Reference (1) and page 6, II B

(QTH)	BWG 12 - .109
	13 - .095
	14 - .083
	15 - .072
	16 - .065
	17 - .058
	18 - .049

4. Material and Gage Factors: Reference (1) and page 6, II B

(QCU)	<u>CU-NI 70-30</u>	<u>CU-NI 90-10</u>	<u>BWG</u>
	.46	.55	12
	.55	.64	13
	.64	.72	14
	.71	.79	15

<u>CU-NI 70-30</u>	<u>CU-NI 90-10</u>	<u>BWG</u>
.76	.84	16
.80	.87	17
.83	.90	18

5. Factors Used in Determining Saturation Pressure of a Saturated

Liquid: Reference (3)

(QPFT)

$$A = 3.2437814$$

$$B = .00586826$$

$$C = 1.1702379E-8$$

$$D = .0021878462$$

$$E = 0.0$$
  

$$A = 3.346313$$

$$B = .0414113$$

$$C = 7.515484E-9$$

$$D = .013794481$$

$$E = 6.56444E-11$$

VI CODING INFORMATION

A. Flow Charts

I

COMMON XMA1TU,GA1TU,D5TU,F2TCLN,XN2TSE,XL1TUI

COMMON F2TUHO,XN2PS,R9SF5,HT1SR,P2BDES,V1WTU

COMMON TE1INJ,XL1TT,D5COND,XL1TUO,QL1TUO

COMMON S2TU,XL1TUE,XN2TUT,D5TUSH,A1TUSH,XL1CON

COMMON R9SW2,TE10,TE1TD,TE1R,W2COND,VL1HW

DIMENSION QTITLE(12)

DIMENSION QAA(9),QCU(7,2),QCF(15),QTH(7)

DIMENSION QPFT(5,2),QMA(2)

DIMENSION QP1(11),QP2(11),QP3(10),QP4(10),QP5(10),QP6(10),QP7(10)  
QP8(10),QP9(10),QP10(10),QP11(10)

SEE DATA STATEMENT

QAA

SEE DATA STATEMENT

QCU

SEE DATA STATEMENT

QCF

SEE DATA STATEMENT

QTH

SEE DATA STATEMENT

QPFT

DATA QAA/35.15789,24.592588,2.1182069,-.3414474,.15741642,  
.3132958E-1,.38658282E-2,-.24901784E-3,.68401559E-5/

DATA QCU/.46,.55,.64,.71,.76,.80,.83,.55,.64,.72,.79,.84,  
.87,.90/

DATA QCF/.65,.7,.75,.798,.843,.886,.926,.963,1.,1.025,  
1.045,1.061,1.076,1.09,1.1/

DATA QTH/.109,.095,.083,.072,.065,.058,.049/

DATA QPFT/3.2437814,.00586826,1.1702379E-8,.0021878462,0.,  
3.346313,.0414113,7.515484E-9,.013794481,6.56444E-11/

DATA QMA/6H 70-30,6H 90-10/

1 FORMAT (12A6)

2 FORMAT (1H1,/,24X,12A6,/, ,13H0INPUT VALUES,//)

3 FORMAT (6E12.6)

5           FORMAT(14HOTUBE MATERIAL,40X,A6/10H TUBE GAGE,30X,F20.0/  
20H TUBE DIAMETER (IN),20X,F20.4)

6           FORMAT (19H CLEANLINESS FACTOR,21X,F20.4/30H NUMBER OF TUBE  
SHEETS PER END,10X,F20.0/38H INEFFECTIVE TUBE LENGTH PER  
END (IN),F22.4)

7           FORMAT(23H TUBE HOLE SPACE FACTOR,17X,F20.4,/17H NUMBER OF  
PASSES,23X,F20.0,/28H STEAM TO CONDENSER (LB/HR),F32.0)

8           FORMAT(43H HEAT REJECTED PER POUND OF STEAM (BTU/LB),F17.2,/30H  
DESIGN BACK PRESSURE (IN HG),F30.2,/39H CIRC WATER  
VELOCITY IN TUBES (FT/SEC,F21.2)

9           FORMAT (37H INJECTION WATER TEMPERATURE (DEG F),F23.2,/39H  
DESIRED OVERALL CONDENSER LENGTH (FT),F21.2,/37H DESIRED  
DIAMETER OF TUBE SHEET (FT),F23.2)

10          FORMAT (36H ORDERED TUBE LENGTH SHORTEST (FT),F24.2,/35H  
ORDERED TUBE LENGTH LONGEST (FT),F25.2)

15          FORMAT (6E20.8)

20          FORMAT (22H0INPUT VALUE P2BDES IS,E15.8,5X,28HSHOULD BE BETWE  
AND 450)

21          FORMAT (22H0INPUT VALUE TE1INJ IS,E15.8,5X,28HSHOULD BE BETWE  
AND 100)

22          FORMAT (21H0INPUT VALUE GAITU IS,E15.8,5X,27HSHOULD BE BETWEE  
AND 18)

23          FORMAT (22H0INPUT VALUE XMA1TU IS,E15.8,5X,16HSHOULD BE 1 OR

24          FORMAT (19H0XL1TUI IS NEGATIVE,E15.8)

25          FORMAT (22H0INPUT VALUE XN2TSE IS,E15.8,5X,16HSHOULD BE 1 OR

26          FORMAT (19H0F2TUHO IS NEGATIVE,E15.8)

27          FORMAT (1H0,30X,36HTERMINAL TEMP DIFF LESS THAN 5 DEG F)

28          FORMAT (36H0DIAMETER OF TUBE SHEET IS TOO LARGE)

39          FORMAT (14H1OUTPUT VALUES,/,38H0TEMPERATURE SATURATED  
LIQUID (DEG F),F22.4)

40          FORMAT (26H0ORDERED TUBE LENGTH (FT),4X,10F9.2)

41          FORMAT (27H0TUBE SURFACE AREA (SQ FT),3X,10F9.0)

42          FORMAT (28H0EFFECTIVE TUBE LENGTH (FT),2X,10F9.2)

43          FORMAT (16H0NUMBER OF TUBES,14X,10F9.0)

44          FORMAT (26H0TUBE SHEET DIAMETER (FT),4X,10F9.2)

45          FORMAT (25H0TUBE SHEET AREA (SQ FT),5X,10F9.2)

46          FORMAT (31H0OVERALL CONDENSER LENGTH (FT),F8.2,9F9.2)

```

47     FORMAT (20H0CIRCULATING WATER REQD (GPM),10F9.0)
48     FORMAT (22H0CIRC WATER OUTLET TEMP (DEG F),F7.2,9F9.2)
49     FORMAT (28H0TERMINAL TEMP DIFF (DEG F),2X,10F9.2)
50     FORMAT (30H0CIRC WATER TEMP RISE (DEG F),10F9.2)

      CALL CAMRAV (35)

```

READ INPUT

```

SEE NEXT STATEMENT                                QTITLE

      ***READ(5,1)QTITLE
      ***READ(5,3)XMA1TU,GA1TU,D5TU,F2TCLN,XN2TSE,XL1TUI
      ***READ(5,3)F2TUHO,XN2PS,R9SF5,HT1SR,P2BDES,V1WTU
SEE NEXT STATEMENT                                QL1TUO

      ***READ(5,3)TE1INJ,XL1TT,D5COND,XL1TUO,QL1TUO

```

PRINT INPUT

```

      ***WRITE(6,2)QTITLE
      I=XMA1TU
      ***WRITE(6,5)QMA(I),GA1TU,D5TU
      ***WRITE(6,6)F2TCLN,XN2TSE,XL1TUI
      ***WRITE(6,7)F2TUHO,XN2PS,R9SF5
      ***WRITE(6,8)HT1SR,P2BDES,V1WTU
      ***WRITE(6,9)TE1INJ,XL1TT,D5COND
      ***WRITE(6,10)XL1TUO,QL1TUO
SEE NEXT STATEMENT                                MPTS

      I
      I MPTS =0
      I P2BDES =P2BDES*.49115
      I
      I

```

I

COMPUTE TEMPERATURE OF SATURATED LIQUID

```

      I
      I
      . * * .
    . * * IF * .
  * * (P2BDES-.2) *
I * . * . * I
I * . * . * I
I * . * . * I
- I      0 I      + I
-----
I 105 I      I 106 I      I 106 I
-- --

```

105 \*\*\*WRITE(6,20)P2BDES

STOP

```

      I
      I
      . * * .
    . * * IF * .
  * * (P2BDES-450.) *
I * . * . * I
I * . * . * I
I * . * . * I
- I      0 I      + I
-----
I 109 I      I 105 I      I 105 I
-- --

```

```

      I
109      I TE1SAT =QAA(1)      I

```

```

      I
      SEE NEXT STATEMENT      QT1

```

```

      I
      I QT1 =1.      I

```

```

      I
      SEE NFXT STATEMENT      QT2

```

```

      I
      I QT2 =ALOG(10.*P2BDES)      I

```



```

120      I K      =TE1INJ/5.-5.          I
        I QT1    =(K+5)*5              I
        I F2TEC=QCF(K)+(QCF(K+1)-QCF(K)) I
        I          *(TE1INJ-QT1)*.2     I
        I

```

FIND WALL THICKNESS

```

        I
        I
        . * . * .
        * * IF * *
        * (GA1TU-12.) *
        I * . * * I
        I * . * * I
        I * . * * I
        - I      0 I      + I
        ----
        I 121 I      I 122 I      I 122 I
        ---*--

```

```

121      ***WRITE(6,22)GA1TU

```

STOP

```

122      I
        I
        . * . * .
        * * IF * *
        * (GA1TU-18.) *
        I * . * * I
        I * . * * I
        I * . * * I
        - I      0 I      + I
        ----
        I 125 I      I 125 I      I 121 I
        ---

```

```

        I
125      I K      =GA1TU-11.          I
        I TH1TU=QTH(K)              I
        I

```

FIND MATERIAL FACTOR

```

      I
      I
      . * * .
    . * * IF * .
  * (XMA1TU-1.) *
  I * . * * I
  I * . * * I
  I * . * * I
- I      0 I      + I
-----
I 126 I      I 128 I      I 127 I
---+-

```

126 \*\*\*WRITE(6,23)XMA1TU

STOP

```

      I
      I
      . * * .
    . * * IF * .
  * (XMA1TU-2.) *
  I * . * * I
  I * . * * I
  I * . * * I
- I      0 I      + I
---*-
I 126 I      I 128 I      I 126 I
---*-

```

```

      I
      I L      =XMA1TU      I
      I F2MG =QCU(K,L)      I
      I

```

COMPUTE INEFFECTIVE TUBE LENGTH PER END

```

      I
      I
      . * * .
    . * * IF * .
  * (XL1TUI) *
  I * . * * I
  I * . * * I
  I * . * * I
- I      0 I      + I
-----
I 140 I      I 145 I      I 150 I
-----

```

140 \*\*\*WRITE(6,24)XL1TUI

```

          STOP
          I
          I
145      . * * .
        . * * IF * .
        * (XN2TSE-1.) *
          I * . * * I
          I * . * * I
          I * . * * I
        - I      0 I      + I
        ----
I 146 I      I 147 I      I 148 I
---*--

```

```

146      ***WRITE(6,25)XN2TSE

```

```

          STOP
          I
147      I XL1TUI =1.0625
          I
          I
          --
          I 150 I
          --

```

```

          I
          I
148      . * * .
        . * * IF * .
        * (XN2TSE-2.) *
          I * . * * I
          I * . * * I
          I * . * * I
        - I      0 I      + I
        ----
I 146 I      I 149 I      I 146 I
--- --

```

```

          I
149      I XL1TUI =6.25
          I

```

COMPUTE TUBE HOLE SPACE FACTOR

```

150      . * * .
      . * * IF * .
      * (F2TUHO) *
      I * . * * I
      I * . * * I
      - I      0 I      + I
      ----
      I 151 I      I 152 I      I 160 I
      --*+

```

```

151      ***WRITE(6,26)F2TUHO

```

```

      STOP

```

```

152      I
      I
      . * * .
      . * * IF * .
      * (P2BDES-1.25) *
      I * . * * I
      I * . * * I
      I * . * * I
      - I      0 I      + I
      ---+--
      I 153 I      I 153 I      I 154 I
      -- -

```

```

153      I
      I F2TUHO =.22      I
      I
      I
      --
      I 160 I
      --

```

```

154      I
      I F2TUHO =.24      I
      I

```

```

      COMPUTE HEAT TRANSFER COEFFICIENT

```

```

160      I
      I
      . * * .
      . * * IF * .
      * (D5TU-.875) *
      I * . * * I

```

```

      I      * .      . *      I
      I      * . *      I
    - I      0 I      + I
  ---*---
  I 162 I      I 161 I      I 161 I
  ---

```

```

      I
161      I C1HEAT =263.      I

```

```

      I
      I
      --
      I 180 I
      --

```

```

      I
162      I C1HEAT =270.      I

```

```

      I

```

COMPUTE GPM / TUBE / 1 FPS VELOCITY

```

      I
180      I QT2 =D5TU-2.*TH1TU      I
      I QT1 =QT2*QT2      I
      I R1V6TU =2.4479922*QT1      I

```

```

      I

```

COMPUTE TUBE CONSTANT

```

      I
      I C9TU) =.10694444*D5TU/QT1      I

```

```

      I

```

SEE NEXT STATEMENT

```

      I
      I QT3 =C1HEAT*C9TU*F2MG*F2TEC*F2TCLN      I

```

```

I      /500.      I
      I

```

IF CONTRACT DESIGN FIND ORDERED TUBE LENGTH

```

      I
      I
      . * * .
    * * * * *
  I * * * * * I
  I * * * * * I
  I * * * * * I
- I * * * * * + I
-----
I 200 I      I 200 I      I 190 I
----+

```

```

      I
190      I XL1TUO =XL1TT-7.5      I
      I

```

COMPUTE EFFECTIVE TUBE LENGTH

```

      I
200      I XL1TUE =(XL1TUO-XL1TUI/6.)*XN2PS      I
      I

```

COMPUTE CIRC. WATER OUTLET TEMP.

```

      I
      I TE1O =TE1SAT-(TE1SAT-TE1INJ)/EXP(XL1TUE
      I      *QT3/SQRT(V1WTU))      I

```

COMPUTE CIRC. WATER TEMP. RISE

```
      I
      I TE1R =TE10-TE1INJ      I
      I
```

COMPUTE TERMINAL TEMP. DIFF.

```
      I
      I TE1TD=TE1SAT-TE10      I
      I
```

STOP PROGRAM IF TERMINAL TEMP. DIFF. LESS THAN 5 DEGREE

```
      I
      I
      . * . * .
      * (TE1TD.GE.5.) *
ON I I OFF
  I I
-----**
I GOTO102 I I
-----**
```

\*\*\*WRITE(6,27)

```
      I
      I XL1TT=-1.      I
      I R9SW2=0.      I
      I S2TU =0.      I
      I XN2TUT =0.      I
      I A1TUSH =0.      I
      I D5TUSH =0.      I
```

```
I XL1CON =0. I
I W2COND =0. I
I VL1HW=0. I
```

```
I
I
--
I 300 I
--
```

COMPUTE CIRC. WATER REQ

```
I
202 I R9SW2=R9SF5*HT1SR/(500.*TE1R) I
I
```

COMPUTE TUBE SURFACE

```
I
I S2TU =XL1TUE*R9SW2*C9TU/V1WTU I
I
```

COMPUTE NUMBER OF TUBES

```
I
I L =(R9SW2*XN2PS/(R1V6TU*V1WTU)) I
I +1. I
I XN2TIT =L I
I
```



```
                I
215      I XL1CON =XL1TUO+D5TUSH                I
```

```
                I
                I
                I
220      . * * *
      . * * * IF * *
    * * * * (XL1TT) * *
  I * * * * * * * I
  I * * * * * * * I
  I * * * * * * * I
- I * * * * * * * + I
-----
I 350 I      I 300 I      I 221 I
-----
```

```
                I
                I
                I
221      . * * *
      . * * * IF * *
    * * * * (XL1CON-XL1TT) * *
  I * * * * * * * I
  I * * * * * * * I
  I * * * * * * * I
- I * * * * * * * + I
-----
I 222 I      I 222 I      I 350 I
-----
```

```
                I
222      I MPTS =0                                I
                I
```

STORE OUTPUT VALUES

```
                I
300      I MPTS =MPTS+1                            I
```

```
                I
SEE NEXT STATEMENT                                QP1
```

```
                I
      I GP1(MPTS) =XL1TUO                            I
```

```
                I
SEE NEXT STATEMENT                                QP2
```

I		
I QP2(MPTS) =S2TU	I	
I		
SEE NEXT STATEMENT		QP3
I		
I QP3(MPTS) =XL1TUE	I	
I		
SEE NEXT STATEMENT		QP4
I		
I QP4(MPTS) =XN2TUT	I	
I		
SEE NEXT STATEMENT		QP5
I		
I QP5(MPTS) =D5TUSH	I	
I		
SEE NEXT STATEMENT		QP6
I		
I QP6(MPTS) =A1TUSH	I	
I		
SEE NEXT STATEMENT		QP7
I		
I QP7(MPTS) =XL1CON	I	
I		
SEE NEXT STATEMENT		QP8
I		
I QP8(MPTS) =R9SW2	I	
I		
SEE NEXT STATEMENT		QP9
I		
I QP9(MPTS) =TE10	I	

I  
SEE NEXT STATEMENT

QR10

I  
I QP10(MPTS) =TE1TD

I

I  
SEE NEXT STATEMENT

QP11

I  
I QP11(MPTS) =TE1R

I

I  
I  
I  
\* \* \*  
\* \* IF \* \*  
\* (MPTS-10) \*  
I \* \* \* \* I  
I \* \* \* \* I  
I \* \* \* \* I  
- I 0 I + I  
-----  
I 309 I I 350 I I 350 I  
---\*\*

309

I  
I  
I  
\* \* \*  
\* \* IF \* \*  
\* (XL1TT) \*  
I \* \* \* \* I  
I \* \* \* \* I  
I \* \* \* \* I  
- I 0 I + I  
-----  
I 350 I I 310 I I 320 I  
--- -

310

I  
I XL1TUO =XL1TUO+.5

I

I  
I  
I  
\* \* \*  
\* \* IF \* \*  
\* (XL1TUO-QL1TUO) \*  
I \* \* \* \* I  
I \* \* \* \* I  
I \* \* \* \* I  
- I 0 I + I  
-----  
I 200 I I 200 I I 350 I  
-----  
40

```

320      I
      . * * .
      . * IF * .
      * (XL1CON-XL1TT) *
      I * . * * I
      I * . * * I
      I * . * * I
      - I      0 I      + I
      ----
      I 321 I      I 350 I      I 350 I
      ----

```

```

      I
321      I XL1TUO =XL1TUO+.5      I
      I
      I
      --
      I 200 I
      --

```

PRINT OUTPUT

```

350      ***WRITE(6,40)(QP1(K),K=1,MPTS)
      ***WRITE(6,41)(QP2(K),K=1,MPTS)
      ***WRITE(6,42)(QP3(K),K=1,MPTS)
      ***WRITE(6,43)(QP4(K),K=1,MPTS)
      ***WRITE(6,44)(QP5(K),K=1,MPTS)
      ***WRITE(6,45)(QP6(K),K=1,MPTS)
      ***WRITE(6,46)(QP7(K),K=1,MPTS)
      ***WRITE(6,47)(QP8(K),K=1,MPTS)
      ***WRITE(6,48)(QP9(K),K=1,MPTS)
      ***WRITE(6,49)(QP10(K),K=1,MPTS)
      ***WRITE(6,50)(QP11(K),K=1,MPTS)
      I
      I
      . * * .
      . * IF * .
      * (XL1TT) *
      41

```

```

      . I * .
      I   * .
      I     * . *
      - I       0 I       + I
      ---
      I 1000I       I 400 I       I 500 I
      -----

```

PLOT DIAMETER VERSUS LENGTH

```

      I
400      I QT1 =QP5(1)      I
      I QT2 =QP5(1)      I
      I
      SEE NEXT STATEMENT      QLL
      I
      I QLL =QP7(1)      I
      I
      SEE NEXT STATEMENT      QLR
      I
      I QLR =QP7(1)      I
      I
      I
      + DO      +
      + DO      +
      + K=2,MPTS      +
      +      +
      I
      I
      I QT1 =AMIN1(QT1,QP5(K))      I
      I QT2 =AMAX1(QT2,QP5(K))      I
      I QLL =AMIN1(QLL,QP7(K))      I
      I
      I
410 ++++++I QLR =AMAX1(QLR,QP7(K))      I
      I
      SEE NEXT STATEMENT      QDX

```

SEE NEXT STATEMENT MERR

CALL DXDYV (1,QLL,QLR,QDX,N,I,NX,20.,MERR)

SEE NEXT STATEMENT QDY

CALL DXDYV (2,QT1,QT2,QDY,M,J,NY,20.,MERR)

CALL GRID1V (3,QLL,QLR,QT1,QT2,QDX,QDY,N,M,-I,-J,NX,NY)

CALL PRINTV (-11,11HLENGTH FT.,492,4)

CALL PRINTV (72,QTITLE,244,1012)

CALL APRNTV (0,-14,-13,13HDIAMETER FT.,4,584)

SEE NEXT STATEMENT MX1

I

I MX1 =NXV(QP7(1)) I

I

SEE NEXT STATEMENT MY1

I

I MY1 =NYV(QP5(1)) I

I

I

+ DO +  
+++++ 420 +  
+ + K=2,MPTS +  
+ + +

I

SEE NEXT STATEMENT MX2

I

I MX2 =NXV(QP7(K)) I

I

SEE NEXT STATEMENT MY2

I

I MY2 =NYV(QP5(K)) I

I

CALL LINEV (MX1,MY1,MX2,MY2)

I

```

+
+      I MX1  =MX2      I
+
+      I
+
420 ++++++I MY1  =MY2      I
      I
      I
      --
      I 1000I
      --

```

CHECK CONDENSER WIDTH

```

500
      I
      I
      . * * * *
      . * * * * IF * *
      * (D5COND-QP5(1)) *
      I . * * * * I
      I * * * * I
      I * * * * I
      - I      0 I      + I
      ----
      I 501 I      I 510 I      I 510 I
      -- *

```

```

501      ***WRITE'6,28)
      I
      --
      I 1000I
      --

```

PLOT HEAT LOAD VERSUS ABSOLUTE PRESSURE

```

      I
510      I QT1  =R9SF5*HT1SR      I
      I QT2  =QT1/50.      I
      I QLL  =QT1*.1      I

```

```

I QT1 =QLL+QT1 I
I
CALL GRID1V (3,QLL,QT1,10.,0.,QT2,.2,5,5,-10,-5,-6,2)
CALL PRINTV (72,QITITLE,244,1020)
CALL PRINTV (-17,17HHEAT LOAD BTU/HR,460,4)
CALL APKNIV (0,-14,-24,24HABSOLUTE PRESSURE IN HG,4,656)
CALL PRINTV (-19,19HCIRC WATER VELOCITY,816,1006)
CALL PRINTV (-17,17HIN TUBES (FT/SEC),824,990)

SEE NEXT STATEMENT QTC
I
I QTC =647.27 I
I
SEE NEXT STATEMENT QPC
I
I QPC =6527.90844 I
I MPTS =11 I
I MX1 =V1WTU I
I V1WTU=MX1 I
I
520 I QT1 =EXP(QT3*XL1TUE/SQRT(V1WTU)) I
I R9SW2=XN2TUT*R1V6TU*V1WTU/XN2PS I
I QT2 =0. I
I
I
+ DO +
+++++ 550 +
+ I=1,MPTS +
+ + +
+ I
+ I
+
I QT2 =QT2+QLL I
+ I QP1(I) =QT2 I
+ I TE10 =TE1INJ+QT2/(500.*R9SW2) I
+ I TE1SAT =(QT1*TE10-TE1INJ)/(QT1 I
+ I -1.) I
+
+ I
+ I
+ I
+ . * * * .
+ * * IF * * 45

```

```

+      * (TE1SAT-200.) *
+      I * . * . * . * I
+      I * . * . * . * I
+      I * . * . * . * I
+      - I      0 I      + I
+      -- -
+ I 530 I      I 531 I      I 531 I
+ ---*+
+
+      I
+
+      I L      =1
530 +      I
+      I
+      --
+      I 535 I
+      -*
+
+      I
+
+      I L      =2
531 +      I
+      I
+
+      I TE1SAT =(TE1SAT-32.)*5./9.+273.16
535 +      I QDX =QTC-TE1SAT
+      I QDY =QDX/TE1SAT*(((QPFT(3,L)+QPFT(5,L)
+      I      *QDX)*QDX*QDX+
+      I      QPFT(2,L))*QDX+QPFT(1,L))/(1.+QPFT(4,L)*QDX)
+      I P2BDES =QPC/10.**QDY
+      I
+      I
+
+      I
550 ++++++I QP2(I) =P2BDES
+      I MX1 =NXV(QP1(1))
+      I MY1 =NYV(QP2(1))
+      I
+      I
+      I
+      +
+      + DO
+++++*+
+      + 560
+      + K=2,MPTS
+      +
+      I
+      I
+
+      I MX2 =NXV(QP1(K))
+      I
+      I
+      I
+      . * * * .
+      . * * * .
+      * IF *
+      * (QP2(K)-10.) *
+      I * . * . * . * I
+      I * . * . * . * I

```

```

+   I           * . *           I
+  - I           0 I           + I
+
+ I 555 I       I 555 I       I 561 I
+
+           I
+
555 +   I MY2 =NYV(QP2(K))           I
+
+           I
+   CALL LINEV (MX1,MY1,MX2,MY2)
+           I
+   I MX1 =MX2           I
+
+           I
560 ++++++I MY1 =MY2           I
+
+           I
561   I MY1 =MY1+3           I
+
+           I
+   CALL LABLV (V1WTU,MX1,MY1,3,1,3)
+           I
+   I MX1 =MX1+24           I
+
+           I
+   CALL PRINTV (-4,4H FPS,MX1,MY1)
+           I
+   I V1WTU=V1WTU-1.           I
+
+           I
+           I
+           I
+           * . * . * .
+           * . IF * . * .
+           * (V1WTU-3.) *
+ I * . * . * . * I
+ I * . * . * . * I
+ I * . * . * . * I
+ - I           0 I           + I
+
+ I 1000I       I 520 I       I 520 I
+
1000   CALL FVEFN (1,16)
+
+   CALL MZEFN (1,1)
+
+   STOP
END
*   *

```

## B. Program Listing

```

C  I.  IDENTIFICATION
C
C  A.  TITLE - STEAM CONDENSER DESIGN
C      1.  FORTRAN IV DECKNAME - COND
C      2.  REVISION - A - ORIGINAL ISSUE
C  B.  ABSTRACT - THIS PROGRAM CALCULATES ALL THE NECESSARY
C      INFORMATION REQUIRED FOR THE SELECTION OF MAIN OR AUXILIARY
C      STEAM CONDENSERS TO EITHER PRELIMINARY OR CONTRACT DESIGN
C      REQUIREMENTS.
C      FOR PRELIMINARY DESIGN A GRAPH IS ALSO PROVIDED WHICH
C      RELATES CONDENSER OVERALL LENGTH WITH TUBE SHEET DIAMETER
C      FOR A SPECIFIED SET OF DESIGN CONDITIONS. FOR CONTRACT
C      DESIGN A GRAPH RELATING CONDENSER ABSOLUTE PRESSURE AND
C      INCREMENTS OF HEAT REJECTION AT INTEGER CIRCULATING WATER
C      VELOCITIES IS ALSO PROVIDED FOR ANALYSIS OF PART LOAD
C      PERFORMANCE.
C  C.  INPUT / CALCULATED ITEMS / OUTPUT
C      1.  INPUT
C          TUBE MATERIAL                XMA1TU
C          TUBE GAGE                     GA1TU
C          TUBE OUTSIDE DIAMETER (INCHES) D5TU
C          NUMBER OF PASSES              XN2PS
C          CLEANLINESS FACTOR            F2TCLN
C          NUMBER OF TUBE SHEETS PER END  XN2TSE
C          INEFFECTIVE TUBE LENGTH PER END (INCHES) XL1TUI
C          TUBE HOLE SPACE FACTOR        F2TUHO
C          STEAM FLOW TO CONDENSER (LB/HR) R9SF5
C          HEAT REJECTED PER POUND OF STEAM (BTU/LB) HT1SR
C          DESIGN BACK PRESSURE (INCHES - HG) P2BDES
C          INJECTION WATER TEMPERATURE (DEG F) TE1INJ
C          OVERALL CONDENSER LENGTH (FT) XL1TT
C          DESIRED DIAMETER OF TUBE SHEET (FT) D5COND
C          CIRCULATING WATER VELOCITY IN TUBES (FT/SEC) V1WTU
C          ORDERED TUBE LENGTH SHORTEST  XL1TUO
C          ORDERED TUBF LENGTH LONGEST    QL1TUO
C      2.  INTERNAL VALUES
C          TUBE WALL THICKNESS            TH1TU
C          BASIC HEAT TRANSFER COEFFICIENT C1HEAT
C          TUBE CONSTANT                  C9TU
C          MATERIAL AND GAGE FACTOR       F2MG
C          TEMPERATURE CORRECTION FACTOR F2TEC
C          GPM / 1 FPS / TUBE             R1V6TU
C      3.  OUTPUT
C          TEMPERATURE SATURATED LIQUID  TE1SAT
C          ORDERER TUBE LENGTH            XL1TUO
C          TUBE SURFACE AREA              S2TU
C          EFFECTIVE TUBE LENGTH          XL1TUE
C          NUMBER OF TUBES                XN2TUT
C          TUBE SHEET DIAMETER            D5TUSH
C          TUBE SHEET AREA                A1TUSH
C          OVERALL CONDENSER LENGTH       XL1CON
C          CIRCULATING WATER REQUIRED (GPM) R9SW2
C          CIRCULATING WATER OUTLET TEMP. TE1O
C          TERMINAL TEMPERATURE DIFF.    TE1TD
C          CIRCULATING WATER TEMPERATURE RISE TE1R
C  D.  AUTHOR/DATE
C      MAXINE BOTTING      DENIS KELLY      DECEMBER 1965
C  E.  ORGANIZATION
C      COMPUTER-AIDED SHIP DESIGN DIVISION, CODE 850,
C      DAVID TAYLOR MODEL BASIN
C  F.  COMPUTER/SOURCE LANGUAGE

```

```

C      - IBM 7090      FORTRAN IV
C      G. REFERENCE TO DOCUMENTATION
C      DTMB REPORT 2255 OF JULY 1966
C      H. SECURITY CLASSIFIED
C      UNCLASSIFIED
C      I. ESTIMATED RUNNING TIME
C      1 1/2 MINUTES
COMMON XMA1TU,GAI1TU,D5TU,F2TCLN,XN2TSE,XL1TUI
COMMON F2TUHO,XN2PS,R9SF5,HT1SR,P2BDES,V1WTU
COMMON TE1INJ,XL1TT,D5COND,XL1TUO,QL1TUO
COMMON S2TU,XL1TUE,XN2TUT,D5TUSH,A1TUSH,XL1CON
COMMON R9SW2,TE1O,TE1TD,TE1R,W2COND,VL1HW
DIMENSION QTITLE(12)
DIMENSION QMA(2)
DIMENSION QAA(9),QCU(7,2),QCF(15),QTH(7)
DIMENSION QPFT(5,2)
DIMENSION QP1(11),QP2(11),QP3(10),QP4(10),QP5(10),QP6(10),QP7(10),
1QP8(10),QP9(10),QP10(10),QP11(10) 456 BYTES
C      SEE DATA STATEMENT                                QAA
C      SEE DATA STATEMENT                                QCU
C      SEE DATA STATEMENT                                QCF
C      SEE DATA STATEMENT                                QTH
C      SEE DATA STATEMENT                                QPFT
DATA QAA/35.15789,24.592588,2.1182069,-.3414474,.15741642,
1-.3132958E-1,.38658282E-2,-.24901784E-3,.68401559E-5/
DATA QCU/.46,.55,.64,.71,.76,.80,.83,.55,.64,.72,.79,.84,
1.87,.90/
DATA QCF/.65,.7,.75,.798,.843,.886,.926,.963,1.,1.025,
11.045,1.061,1.076,1.09,1.1/
DATA QTH/.109,.095,.083,.072,.065,.058,.049/
DATA QPFT/3.2437814,.00586826,1.1702379E-8,.0021878462,0.,
13.346313,.0414113,7.515484E-9,.013794481,6.56444E-11/
DATA QMA/6H 70-30,6H 90-10/
1 FORMAT (12A6)
2 FORMAT (1H1,/,24X,12A6,/,13H0INPUT VALUES,/)
3 FORMAT (6E12.6)
5 FORMAT (14H0TUBE MATERIAL,40X,A6 /10H TUBE GAGE,30X,F20.0,/20H
1TUBE DIAMETER (IN),20X,F20.4)
6 FORMAT (19H CLEANLINESS FACTOR,21X,F20.4,/30H NUMBER OF TUBE SHEET
1S PER END,10X,F20.0,/38H INEFFECTIVE TUBE LENGTH PER END (IN),F22
2.4)
7 FORMAT (23H TUBE HOLE SPACE FACTOR,17X,F20.4,/17H NUMBER OF PASSES
1,23X,F20.0,/28H STEAM TO CONDENSER (LB/HR),F32.0)
8 FORMAT (43H HEAT REJECTED PER POUND OF STEAM (BTU/LB),F17.2,/30H
1DESIGN BACK PRESSURE (IN HG),F30.2 ,/39H CIRC WATER VELOCITY IN T
2UBES (FT/SEC),F21.2)
9 FORMAT (37H INJECTION WATER TEMPERATURE (DEG F),F23.2,/39H DESIRE
1D OVERALL CONDENSER LENGTH (FT),F21.2,/37H DESIRED DIAMETER OF TU
2BE SHEET (FT),F23.2)
10 FORMAT (36H ORDERED TUBE LENGTH SHORTEST (FT),F24.2,/35H ORDERED
1 TUBE LENGTH LONGEST (FT),F25.2)
15 FORMAT (6E20.8)
20 FORMAT (22H0INPUT VALUE P2BDES IS,E15.8,5X,28HSHOULD BE BETWEEN .2
1 AND 450)
21 FORMAT (22H0INPUT VALUE TE1INJ IS,E15.8,5X,28HSHOULD BE BETWEEN 30
1 AND 100)
22 FORMAT (21H0INPUT VALUE GAI1TU IS,E15.8,5X,27HSHOULD BE BETWEEN 12
1AND 18)
23 FORMAT (22H0INPUT VALUE XMA1TU IS,E15.8,5X,16HSHOULD BE 1 OR 2)
24 FORMAT (19H0XL1TUI IS NEGATIVE,E15.8)

```

25 FORMAT (22H0INPUT VALUE XN2TSE IS,E15.8,5X,16HSHOULD BE 1 OR 2)  
 26 FORMAT (19H0F2TUHO IS NEGATIVE,E15.8)  
 27 FORMAT (1H0,30X,36HTERMINAL TEMP DIFF LESS THAN 5 DEG F)  
 28 FORMAT (36H0DIAMETER OF TUBE SHEET IS TOO LARGE)  
 39 FORMAT (14H1OUTPUT VALUES, //38HOTEMPERATURE SATURATED LIQUID (DEG  
 1 F),F22.4)  
 40 FORMAT (26H0ORDERED TUBE LENGTH (FT),4X,10F9.2)  
 41 FORMAT (27HOTUBE SURFACE AREA (SQ FT),3X,10F9.0)  
 42 FORMAT (28H0EFFECTIVE TUBE LENGTH (FT),2X,10F9.2)  
 43 FORMAT (16H0NUMBER OF TUBES,14X,10F9.0)  
 44 FORMAT (26HOTUBE SHEET DIAMETER (FT),4X,10F9.2)  
 45 FORMAT (25HOTUBE SHEET AREA (SQ FT),5X,10F9.2)  
 46 FORMAT (31H0OVERALL CONDENSER LENGTH (FT),F8.2,9F9.2)  
 47 FORMAT (30H0CIRCULATING WATER REQD (GPM),10F9.0)  
 48 FORMAT (32H0CIRC WATER OUTLET TEMP (DEG F),F7.2,9F9.2)  
 49 FORMAT (28HOTERMINAL TEMP DIFF (DEG F),2X,10F9.2)  
 50 FORMAT (30H0CIRC WATER TEMP RISE (DEG F),10F9.2)  
 CALL CAMRAV (35)

C  
 C READ INPUT  
 C  
 C SEE NEXT STATEMENT QTITLE  
 C READ(5,1)QTITLE  
 C READ(5,3)XMA1TU,GA1TU,D5TU,F2TCLN,XN2TSE,XL1TUI  
 C READ(5,3)F2TUHO,XN2PS,R9SF5,HT1SR,P2BDES,V1WTU  
 C SEE NEXT STATEMENT QL1TUO  
 C READ(5,3)TE1INJ,XL1TT,D5COND,XL1TUO,QL1TUO  
 C  
 C PRINT INPUT  
 C  
 C WRITE(6,2)QTITLE  
 C I=XMA1TU  
 C WRITE(6,5)QMA(I),GA1TU,D5TU  
 C WRITE(6,6)F2TCLN,XN2TSE,XL1TUI  
 C WRITE(6,7)F2TUHO,XN2PS,R9SF5  
 C WRITE(6,8)HT1SR,P2BDES,V1WTU  
 C WRITE(6,9)TE1INJ,XL1TT,D5COND  
 C WRITE(6,10)XL1TUO,QL1TUO  
 C SEE NEXT STATEMENT MPTS  
 C MPTS=0  
 C P2BDES=P2BDES\*.49115  
 C  
 C COMPUTE TEMPERATURE OF SATURATED LIQUID  
 C  
 C IF(P2BDES-.2) 105,106,106  
 105 WRITE(6,20)P2BDES  
 C STOP  
 106 IF(P2BDES-450.) 109,105,105  
 109 TE1SAT=QAA(1)  
 C SEE NEXT STATEMENT QT1  
 C QT1=1.  
 C SEE NEXT STATEMENT QT2  
 C QT2=ALOG(10.\*P2BDES)  
 C DO 110 K=2,9  
 C QT1=QT1\*QT2  
 110 TE1SAT=TE1SAT+QAA(K)\*QT1  
 C WRITE (6,39)TE1SAT  
 C  
 C COMPUTE CIRC WATER CORRECTION FACTOR  
 C  
 C

```

      IF(TE1INJ-30.) 115,116,116
115 WRITE(6,21)TE1INJ
      STOP
116 IF(TE1INJ-100.) 120,120,115
120 K=TE1INJ/5.-5.
      QT1=(K+5)*5
      F2TEC=QCF(K)+(QCF(K+1)-QCF(K))*(TE1INJ-QT1)*.2
C
C   FIND WALL THICKNESS
C
      IF(GA1TU-12.) 121,122,122
121 WRITE(6,22)GA1TU
      STOP
122 IF(GA1TU-18.) 125,125,121
125 K=GA1TU-11.
      TH1TU=QTH(K)
C
C   FIND MATERIAL FACTOR
C
      IF(XMA1TU-1.) 126,128,127
126 WRITE(6,23)XMA1TU
      STOP
127 IF(XMA1TU-2.) 126,128,126
128 L=XMA1TU
      F2MG=QCU(K,L)
C
C   COMPUTE INEFFECTIVE TUBE LENGTH PER END
C
      IF(XL1TUI) 140,145,150
140 WRITE(6,24)XL1TUI
      STOP
145 IF(XN2TSE-1.) 146,147,148
146 WRITE(6,25)XN2TSE
      STOP
147 XL1TUI=1.0625
      GO TO 150
148 IF(XN2TSE-2.) 146,149,146
149 XL1TUI=6.25
C
C   COMPUTE TUBE HOLE SPACE FACTOR
C
150 IF(F2TUHO) 151,152,160
151 WRITE(6,26)F2TUHO
      STOP
152 IF(P2BDES-1.25) 153,153,154
153 F2TUHO=.22
      GO TO 160
154 F2TUHO=.24
C
C   COMPUTE HEAT TRANSFER COEFFICIENT
C
160 IF(D5TU-.875) 162,161,161
161 C1HEAT=263.
      GO TO 180
162 C1HEAT=270.
C
C   COMPUTE GPM / TUBE / 1 FPS VELOCITY
C
180 QT2=D5TU-2.*TH1TU
      QT1=QT2*QT2

```

```

R1V6TU =2.4479922*QT1
C
C COMPUTE TUBE CONSTANT
C
C9TU=.10694444*D5TU/QT1
C SEE NEXT STATEMENT
C QT3=C1HEAT*C9TU*F2MG*F2TEC*F2TCLN/500.
C
C IF CONTRACT DESIGN FIND ORDERED TUBE LENGTH
C
C IF (XL1TT) 200,200,190
190 XL1TUO=XL1TT-7.5
C
C COMPUTE EFFECTIVE TUBE LENGTH
C
200 XL1TUE=(XL1TUO-XL1TUI/6.)*XN2PS
C
C COMPUTE CIRC. WATER OUTLET TEMP.
C
TE10=TE1SAT-(TE1SAT-TE1INJ)/EXP(XL1TUE*QT3/SQRT(V1WTU))
C
C COMPUTE CIRC. WATER TEMP. RISE
C
TE1R=TE10-TE1INJ
C
C COMPUTE TERMINAL TEMP. DIFF.
C
TE1TD=TE1SAT-TE10
C
C STOP PROGRAM IF TERMINAL TEMP. DIFF. LESS THAN 5 DEGREE
C
C IF (TE1TD.GE.5.) GO TO 202
C WRITE(6,27)
C XL1TT=-1.
C R9SW2=0.
C S2TU=0.
C XN2TUT=0.
C A1TUSH=0.
C D5TUSH=0.
C XL1CON=0.
C W2COND=0.
C VL1HW=0.
C GO TO 300
C
C COMPUTE CIRC. WATER REQ T
C
202 R9SW2=R9SF5*HT1SR/(500.*TE1R)
C
C COMPUTE TUBE SURFACE
C
S2TU=XL1TUE*R9SW2*C9TU/V1WTU
C
C COMPUTE NUMBER OF TUBES
C
L=(R9SW2*XN2PS/(R1V6TU*V1WTU))+1.
C XN2TUT=L
C
C COMPUTE TUBE SHEET AREA
C
QT1=D5TU*D5TU*XN2TUT/(F2TUHO*144.)

```

```

      A1TUSH=.7854*QT1
C
C   COMPUTE TUBE SHEET DIAMETER
C
      D5TUSH=SQRT(QT1)
C
C   COMPUTE OVERALL LENGTH
C
      IF(D5TUSH-7.5) 215,215,210
210 XL1CON=XL1TUO+7.5
      GO TO 220
215 XL1CON=XL1TUO+D5TUSH
220 IF(XL1TT) 350,300,221
221 IF(XL1CON-XL1TT) 222,222,350
222 MPTS=0
C
C   STORE OUTPUT VALUES
C
300 MPTS=MPTS+1
C   SEE NEXT STATEMENT
      QP1(MPTS)=XL1TUO
C   SEE NEXT STATEMENT
      QP2(MPTS)=S2TU
C   SEE NEXT STATEMENT
      QP3(MPTS)=XL1TUE
C   SEE NEXT STATEMENT
      QP4(MPTS)=XN2TUT
C   SEE NEXT STATEMENT
      QP5(MPTS)=D5TUSH
C   SEE NEXT STATEMENT
      QP6(MPTS)=A1TUSH
C   SEE NEXT STATEMENT
      QP7(MPTS)=XL1CON
C   SEE NEXT STATEMENT
      QP8(MPTS)=R9SW2
C   SEE NEXT STATEMENT
      QP9(MPTS)=TE1O
C   SEE NEXT STATEMENT
      QP10(MPTS)=TE1TD
C   SEE NEXT STATEMENT
      QP11(MPTS)=TE1R
      IF(MPTS-10) 309,350,350
309 IF(XL1TT) 350,310,320
310 XL1TUO=XL1TUO+.5
      IF(XL1TUO-QL1TUO) 200,200,350
320 IF(XL1CON-XL1TT) 221,350,350
321 XL1TUO=XL1TUO+.5
      GO TO 200
C
C   PRINT OUTPUT
C
350 WRITE(6,40)(QP1(K),K=1,MPTS)
      WRITE(6,41)(QP2(K),K=1,MPTS)
      WRITE(6,42)(QP3(K),K=1,MPTS)
      WRITE(6,43)(QP4(K),K=1,MPTS)
      WRITE(6,44)(QP5(K),K=1,MPTS)
      WRITE(6,45)(QP6(K),K=1,MPTS)
      WRITE(6,46)(QP7(K),K=1,MPTS)
      WRITE(6,47)(QP8(K),K=1,MPTS)
      WRITE(6,48)(QP9(K),K=1,MPTS)

```

```

WRITE(6,49)(QP10(K),K=1,MPTS)
WRITE(6,50)(QP11(K),K=1,MPTS)
IF(XL1TT) 1000,400,500
C
C   PLOT DIAMETER VERSUS LENGTH
C
400 QT1=QP5(1)
    QT2=QP5(1)
C   SEE NEXT STATEMENT
    QLL=QP7(1)
C   SEE NEXT STATEMENT
    QLR=QP7(1)
    DO 410 K=2,MPTS
    QT1=AMIN1(QT1,QP5(K))
    QT2=AMAX1(QT2,QP5(K))
    QLL=AMIN1(QLL,QP7(K))
410 QLR=AMAX1(QLR,QP7(K))
C   SEE NEXT STATEMENT
C   SEE NEXT STATEMENT
    CALL DXDYV (1,QLL,QLR,QDX,N,I,NX,20.,MERR)
C   SEE NEXT STATEMENT
    CALL DXDYV (2,QT1,QT2,QDY,M,J,NY,20.,MERR)
    CALL GRID1V (3,QLL,QLR,QT1,QT2,QDX,QDY,N,M,-I,-J,NX,NY)
    CALL PRINTV (-11,11HLENGTH FT.,492,4)
    CALL PRINTV (72,QTITLE,244,1012)
    CALL APRNTV (0,-14,-13,13HDIAMETER FT.,4,584)
C   SEE NEXT STATEMENT
    MX1=NXV(QP7(1))
C   SEE NEXT STATEMENT
    MY1=NYV(QP5(1))
    DO 420 K=2,MPTS
C   SEE NEXT STATEMENT
    MX2=NXV(QP7(K))
C   SEE NEXT STATEMENT
    MY2=NYV(QP5(K))
    CALL LINEV (MX1,MY1,MX2,MY2)
    MX1=MX2
420 MY1=MY2
    GO TO 1000
C
C   CHECK CONDENSER WIDTH
C
500 IF(D5COND-QP5(1)) 501,510,510
501 WRITE(6,28)
    GO TO 1000
C
C   PLOT HEAT LOAD VERSUS ABSOLUTE PRESSURE
C
510 QT1=R9SF5*HT1SR
    QT2=QT1/50.
    QLL=QT1*.1
    QF1=QLL+QT1
    CALL GRID1V (3,QLL,QT1,10.,0.,QT2,.2,5,5,-10,-5,-6,2)
    CALL PRINTV (72,QTITLE,244,1020)
    CALL PRINTV (-17,17HHEAT LOAD BTU/HR,460,4)
    CALL APRNTV (0,-14,-24,24HABSOLUTE PRESSURE IN HG,4,656)
    CALL PRINTV (-19,19HCIRC WATER VELOCITY,816,1006)
    CALL PRINTV (-17,17HIN TUBES (FT/SEC),824,990)
C   SEE NEXT STATEMENT
    QTC=647.27

```

```

C      SEE NEXT STATEMENT
      QPC=6527.90844
      MPTS=11
      MX1=V1WTU
      V1WTU=MX1
520   QT1=EXP(QT3*XL1TUE/SQRT(V1WTU))
      R9SW2=XN2TUT*R1V6TU*V1WTU/XN2PS
      QT2=0.
      DO 550 I=1,MPTS
      QT2=QT2+QLL
      QP1(I)=QT2
      TE10=TE1INJ+QT2/(500.*R9SW2)
      TE1SAT=(QT1*TE10-TE1INJ)/(QT1-1.)
      IF(TE1SAT-200.) 530,531,531
530   L=1
      GO TO, 535
531   L=2
535   TE1SAT=(TE1SAT-32.)*5./9.+273.16
      QDX=QTC-TE1SAT
      QDY=QDX/TE1SAT*(((QPFT(3,L)+QPFT(5,L)*QDX)*QDX*QDX+
1QPFT(2,L))*QDX+QPFT(1,L))/(1.+QPFT(4,L)*QDX)
      P2BDES=QPC/10.**QDY
550   QP2(I)=P2BDES
      MX1=NXV(QP1(I))
      MY1=NYV(QP2(I))
      DO 560 K=2,MPTS
      MX2=NXV(QP1(K))
      IF(QP2(K)-10.) 555,555,561
555   MY2=NYV(QP2(K))
      CALL LINEV (MX1,MY1,MX2,MY2)
      MX1=MX2
560   MY1=MY2
561   MY1=MY1+3
      CALL LABLV (V1WTU,MX1,MY1,3,1,3)
      MX1=MX1+24
      CALL PRINTV (-4,4H FPS,MX1,MY1)
      V1WTU=V1WTU-1.
      IF(V1WTU-3.) 1000,520,520
1000  CALL FVEFN (1,16)
      CALL MZEFN(1,1)
      STOP
      END

```

QPC

### C. Special Diagnostics

(1) Design Back Pressure

Input value P2BDES is \_\_\_\_\_

should be between .2 and 450

Program stopped.

(2) Injection water Temperature.

Input value TEINJ is \_\_\_\_\_

Should be between 30 and 100

Program is stopped.

(3) Tube Gage

Input value GAITU is \_\_\_\_\_

Should be between 12 and 18

Program is stopped.

(4) Effective Tube Length

XL1TUE is negative

Program is stopped.

(5) Number of Tube Sheets per end

Input value XN2TSE is \_\_\_\_\_

Should be 1 or 2

Program is stopped.

(6) Tube Material

Input value XMA1TU is \_\_\_\_\_

Should be 1 or 2

Program is stopped.

**(7) Tube Hole Space Factor**

**F2TUHO is negative** •

**Program is stopped.**

**VII. ACKNOWLEDGMENT**

This program utilizes coefficients derived by Raymond W. Yaw,  
Code 6436, NAVSEC.

## **REFERENCES**

- 1. Design Data Sheet DDS4601-1 of 15 October 1953 - Steam Condensers.**
- 2. Military Specification MIL-C-15430G Condensers, Steam Surface, Naval Shipboard.**
- 3. Share Programs C3-WH58-PA-3137 (Westinghouse Corporation Properties of Steam).**



## INITIAL DISTRIBUTION

Copies	Copies
	1 SUPSHIP, NEW ORLEANS
	1 SUPSHIP, CAMDEN
	1 SUPSHIP, SAN FRAN
	1 SUPSHIP, PASCAGOULA
3 NAVSHIPSYSKOM	1 REP SUPSHIP, Sturgeon Bay, WIS
3 Technical Library (Code 2021)	2 MIT
23 NAVSEC	2 UNIV of MICH
1 Ships Research Branch (Code 6341)	2 UNIV of CALIF, Berkeley
10 Computer-Aided Ship Design Cord. (Code 6412)	1 SUPT, USNA
5 Machy Scientific-Research Sect. (Code 6436)	1 CH APPL NAV ARCH USMMA, Dept of Nautical Sci
1 Refrig, A/C, Pump Branch (Code 6649)	1 DIR, DL, SIT
5 Boiler-Heat Exch Branch (Code 6651)	1 WEBB INST
1 Computer Sys Applications Branch (Code 6732)	2 American Bureau of Shipping 45 Broad St, NY
2 NAVSHIPYD BSN	1 CNA, Institute of Naval Studies
2 NAVSHIPYD CHASN	3 ADMIN, MARAD
2 NAVSHIPYD LBEACH	1 Off of Ship Construc
2 NAVSHIPYD MARE	1 R. D. Murphy, Div of Ship Desi
2 NAVSHIPYD PTSMH	1 DIR, NASA
2 NAVSHIPYD PEARL	1 SNAME
3 NAVSHIPYD PHILA	1 USA Corps of Engrs, Phila
1 Boiler Turbine Lab	1 USA Tank Automotive Cntr Warren, Mich Attn H. Smota, RE
2 NAVSHIPYD NORVA	2 COMDT, NSCG
2 NAVSHIPYD PUG	Attn Off of Engrs
2 NAVSHIPYD SFRAN	1 CO, USNROTC&NAVADMIN U, MI
2 CO&DIR, USNASL	1 OinC, PGSCOL, Webb Inst
2 CO&DIR, USNMEL	2 NY State Maritime College
1 CO&DIR, NAVMINDEFLAB	2 Ala DD&Ship Bldg Co, Mobile, Ala
1 CO&DIR, USNUSL	2 American Shipbldg Co, Lorain, Oh
1 CO&DIR, USNEL	2 American Shipbldg Co, Toledo, Oh
1 CO&DIR, USNRDL	2 Guy F. Atkinson Co, Portland, Ore
20 DDC	2 Bath Iron Works Corp
1 SUPSHIP, GROTON	2 Bethlehem Steel Co
1 SUPSHIP, NEWPORT NEWS	2 Avondale Shipyds, Inc
1 SUPSHIP, SEATTLE	2 Boland Machine Mfg, New Orleans
1 SUPSHIP, NEW YORK	2 Christy Corp, Sturgeon, Wisc
1 SUPSHIP, BATH	2 Defoe Shipbldg Co, Bay City, Mich
1 SUPSHIP, JACKSONVILLE	2 Dorchester Shipbldg Corp, Dorchester, NJ
1 SUPSHIP, LONG BEACH	2 Frazier Shipyds Inc, Superior, Wis
	2 Gen Dyn, Quincy, Mass



INITIAL DISTRIBUTION (Cont'd.)

Copies

2 Gen Dyn, Groton  
 2 Gretna Machine&Iron Work Inc,  
     Harvey, Louisiana  
 2 Ingalls Shipbldg Corp  
 2 Levingston Shipbldg Co, Inc  
     Orange, Texas  
 2 Lockheed Shipbldg&Constr Co  
     Seattle, Wash  
 2 Manitowoc Shipbldg, Inc.  
     Manitowac, Wisc  
 2 Marinette Marine Corp  
     Marinette, Wisc  
 2 Marinette Mfg Co  
     Point Pleasant, W. Va  
 2 Md Shipbldg&DD Co  
 2 Nat'l Steel&DD Co  
     San Diego, Calif  
 2 NNSB&DD Co  
 2 NY Shipbldg Corp  
 2 Norfolk Shipbldg&DD Co  
 2 Northwest Marine Iron Works  
     Portland, Ore  
 2 Peterson Builders Inc  
     Sturgeon Bay, Wisc  
 2 Rawls Brothers Contractors Inc  
     Jacksonville, Fla  
 2 Sturgeon Bay Shipbldg&DD Co  
 2 St Louis Shipbldg, Federal Barge, Inc  
     St Louis, Mo  
 2 Southern Shipbldg Corp  
     Slidell, La  
 2 Stephens Marine, Stockton, Calif  
 2 Sun Shipbldg&DD Co  
 2 Tacoma Boatbldg Co, Inc  
     Tacoma, Wash  
 2 Todd Shipyd Corp, San Pedro, Calif  
 2 Todd Shipyd Corp, Seattle, Wash  
 2 Designers & Planners  
     44 Whitehall St, NY  
 2 Freide & Goldman, New Orleans, La  
 2 Gibbs & Cox, Inc. NY  
 2 John J. McMullen  
     17 Battery Pl, NY

Copies

2 J. J. Henry, NY  
 2 W. C. Vickum, Seattle, Wash  
 2 M. Rosenblatt&Sons, NY  
 2 George G. Sharp, NY



DOCUMENT CONTROL DATA - R&D		
<i>(Security classification of title, body of abstract and index annotation must be entered when the overall report is classified)</i>		
1. ORIGINATING ACTIVITY (Corporate author) <b>David Taylor Model Basin Washington, D. C. 20007</b>		2a. REPORT SECURITY CLASSIFICATION <b>UNCLASSIFIED</b>
		2b. GROUP
3. REPORT TITLE <b>COMPUTER PROGRAM DOCUMENTATION STEAM CONDENSER DESIGN</b>		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) <b>Final report</b>		
5. AUTHOR(S) (Last name, first name, initial) <b>Botting, Maxine M. Kelly, Denis W.</b>		
6. REPORT DATE <b>July 1966</b>	7a. TOTAL NO. OF PAGES <b>64</b>	7b. NO. OF REFS <b>3</b>
8a. CONTRACT OR GRANT NO.	9a. ORIGINATOR'S REPORT NUMBER(S) <b>2255</b>	
b. PROJECT NO. <b>SR003-0801</b>		
c. <b>Task</b>	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d. <b>10894</b>		
10. AVAILABILITY/LIMITATION NOTICES <b>Distribution of this document is unlimited.</b>		
11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY <b>NAVSEC</b>	
13. ABSTRACT  <b>This program calculates all the necessary information required for the selection of main or auxiliary steam condensers to either preliminary or contract design requirements.</b>		

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
<p>Computer program Steam condenser design Preliminary design Contract design</p>						

**INSTRUCTIONS**

1. **ORIGINATING ACTIVITY:** Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.
- 2a. **REPORT SECURITY CLASSIFICATION:** Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.
- 2b. **GROUP:** Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.
3. **REPORT TITLE:** Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.
4. **DESCRIPTIVE NOTES:** If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.
5. **AUTHOR(S):** Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.
6. **REPORT DATE:** Enter the date of the report as day, month, year; or month, year. If more than one date appears on the report, use date of publication.
- 7a. **TOTAL NUMBER OF PAGES:** The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.
- 7b. **NUMBER OF REFERENCES:** Enter the total number of references cited in the report.
- 8a. **CONTRACT OR GRANT NUMBER:** If appropriate, enter the applicable number of the contract or grant under which the report was written.
- 8b, 8c, & 8d. **PROJECT NUMBER:** Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.
- 9a. **ORIGINATOR'S REPORT NUMBER(S):** Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.
- 9b. **OTHER REPORT NUMBER(S):** If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).
10. **AVAILABILITY/LIMITATION NOTICES:** Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through \_\_\_\_\_."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through \_\_\_\_\_."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through \_\_\_\_\_."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. **SUPPLEMENTARY NOTES:** Use for additional explanatory notes.
12. **SPONSORING MILITARY ACTIVITY:** Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.
13. **ABSTRACT:** Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U)

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. **KEY WORDS:** Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical content. The assignment of links, roles, and weights is optional.

MIT LIBRARIES DUPL  
3 9080 02753 0788

